

## BJT Circuits at DC

## Kizito NKURIKIYEYEZU, Ph.D.

Active EBJ:
Forward
Biased
CBJ:
Reverse
Biased



FIG 1. Simplified Models for the Operation of the BJT in DC Circuits

## BJT DC analysis steps

Use the following steps when analyzing BJT circuits with DC voltages:
1 Assume that the transistor is operating in active mode.

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3 Check for consistency of results with active-mode operation such as $V_{C E}>V_{\text {CEsat }}$.
4 If it is satisfied, the analysis is over.
5 If not, assume saturation mode and repeat the analysis like active mode.
This analysis is mainly used to identify the operating point.

## Example I

In Fig. 2, if $\beta=100$ and $V_{B E}=0.7 \mathrm{~V}$, which mode is the transistor operating in?

■ Using Kirchhoff's Voltage Law (KVL) on the base-emitter loop (Equation (1))

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\begin{equation*}
4 V=V_{B E}+3.3 \mathrm{k} \Omega I_{E} \tag{1}
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- The base current $I_{B}$ is calculated from its relationship to the emitter current

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I_{B}=\frac{I_{E}}{\beta+1}=9.9 \mu \mathrm{~A} \tag{2}
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- The collector current $I_{C}$ is thus

$$
\begin{equation*}
I_{C}=\beta I_{B}=0.99 \mathrm{~mA} \tag{3}
\end{equation*}
$$



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- $V_{C E}$ is obtained by applying KVL on the CE loop as shown in Equation (4):

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V_{C E}=10 \mathrm{~V}-4.7 \mathrm{kVI}_{C}-3.3 \mathrm{kVI}_{E}=2.047 \mathrm{~V} \tag{4}
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- Since $V_{C E}>V_{C E s a t}$, it is operating in active mode.


FIG 3. Example I

## NPN Common-Emitter circuit

- We will assume that the BEJ is forward biased, so the voltage drop across that junction is the cut-in or turn-on voltage $V_{B E}(\mathrm{on})$.

(a) npn transistor common-emitter

(b) dc equivalent circuit.

FIG 4. Common emitter-Transistor equivalent circuit is shown within the dotted lines with piecewise linear transistor parameters.

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- The base current is given in Equation (5)

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I_{B}=\frac{V_{B B}-V_{B E}(\text { on })}{R_{B}} \tag{5}
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- Equation (5) implies that $V_{B B}>V_{B E}$ (on)—which means that $I_{B}>0$. Otherwise, $V_{B B}<V_{B E}$ (on), the transistor is OFF and $I_{B}=0$.

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- The collector current is given Equation (6)

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- Kirchhoff's voltage law allows to compute $V_{C C}$ and $V_{C E}$

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\begin{align*}
& V_{C C}=I_{C} R_{C}+V_{C E}  \tag{7}\\
& V_{C E}=V_{C C}-I_{C} R_{C} \tag{8}
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■ Equation (8) implicitly assumes that $V_{C E}>V_{B E}(o n)$-which means that the BCJ is reverse biased and the transistor is the forward active mode

## NPN Common-Emitter circuit

- The power dissipated in the transistor is given by Equation

$$
\begin{equation*}
P_{T}=I_{B} V_{B E}(\text { on })+I_{C} V_{C E} \tag{9}
\end{equation*}
$$


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- However, in most cases $I_{C} \gg I_{B}$ and $V_{C E}>V_{B E}(o n)$. Thus, Equation (9) can be simplified as shown in Equation (10)

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P_{T} \approx I_{C} V_{C E} \tag{10}
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■ The approximation in Equation (10), however, is not valid in the saturation mode.

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## Example II

Calculate the base, collector, emitter currents, the $V_{C E}$ voltage and the transistor power dissipation for the common-emitter circuit shown in Fig. 7. Assume $\beta=200$ and $V_{B E}(o n)=0.7 \mathrm{~V}$

■ The base current is found as

$$
\begin{align*}
I_{B} & =\frac{V_{B B}-V_{B E}(\text { on })}{R_{B}} \\
& =\frac{4 V-0.7 V}{20 \mathrm{k}}  \tag{11}\\
& =15 \mu \mathrm{~A}
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& =15 \mu \mathrm{~A}
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- The collector current is

$$
\begin{equation*}
I_{C}=\beta I_{B}=200 \times 15 \mu \mathrm{~A}=3 \mathrm{~mA} \tag{12}
\end{equation*}
$$



FIG 7. Example 2

■ The emitter current is

$$
\begin{equation*}
I_{E}=(1+\beta) I_{B}=3.02 \mathrm{~mA} \tag{13}
\end{equation*}
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FIG 8. Example 2

■ The emitter current is

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- The collector-emitter voltage is

$$
V_{C E}=V_{C C}-I_{C} R_{C}=4 V
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V_{C E}=V_{C C}-I_{C} R_{C}=4 V \tag{14}
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$$

- The power dissipated is

$$
\begin{aligned}
P_{T} & =I_{B} V_{B E}(\text { on })+I_{C} V_{C E} \\
& =0.015 \times 0.7+3 \times 4 \\
& =12 \mathrm{~mW}
\end{aligned}
$$

$$
V_{C C}=10 \mathrm{~V}
$$



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FIG 8. Example 2

- Since $V_{B B}>V_{B E}(o n)$ and $V_{C E}>V_{B E}$ (on), the transistor is biased in the forward-active mode.


## PNP Common-Emitter circuit

- In Fig. 9, the emitter is at ground potential, which means that the polarities of the $V_{B B}$ and $V_{C C}$ power supplies must be reversed compared to those in the npn circuit.

(a) pnp transistor common-emitter

(b) dc equivalent circuit.

FIG 9. Common emitter-Transistor equivalent circuit is shown within the dotted lines with piecewise linear transistor parameters.

## PNP Common-Emitter circuit

- In Fig. 9, the emitter is at ground potential, which means that the polarities of the $V_{B B}$ and $V_{C C}$ power supplies must be reversed compared to those in the npn circuit.
- The analysis proceeds exactly as before, and we can write:

$$
\begin{gather*}
I_{B}=\frac{V_{B} B-V_{E B}(o n)}{R_{B}}  \tag{16}\\
I_{C}=\beta I_{B}  \tag{17}\\
V_{E C}=V_{C C}-I_{C} R_{C}
\end{gather*}
$$

(18) FIG 9. Common emitter-Transistor equivalent circuit is shown within the dotted lines with piecewise linear transistor parameters.

## Example 3

Find $I_{B}, I_{C}, I_{E}$ and $R_{C}$ such that $V_{E C}=\frac{1}{2} V^{+}$for the circuit given in Fig. 10. Assume $\beta=100$ and $V_{E B}(o n)=0.6 \mathrm{~V}$

$$
I_{C}=\beta I_{B}=(100)(5 \mu \mathrm{~A}) \Rightarrow 0.5 \mathrm{~mA}
$$

and the emitter current is

$$
I_{E}=(1+\beta) I_{B}=(101)(5 \mu \mathrm{~A}) \Rightarrow 0.505 \mathrm{~mA}
$$

For a C-E voltage of $V_{E C}=\frac{1}{2} V^{+}=2.5 \mathrm{~V}, R_{C}$ is

$$
R_{C}=\frac{V^{+}-V_{E C}}{I_{C}}=\frac{5-2.5}{0.5}=5 \mathrm{k} \Omega
$$

In this case, $\left(V^{+}-V_{B B}\right)>V_{E B}(o n)$. Also, because VEC > VEB(on), the pnp bipolar transistor is biased in the forward-active mode.


FIG 10. Example 3

The end

