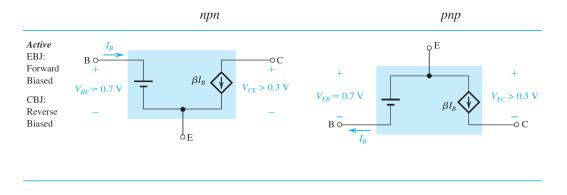


# **BJT Circuits at DC**

# Kizito NKURIKIYEYEZU, Ph.D.



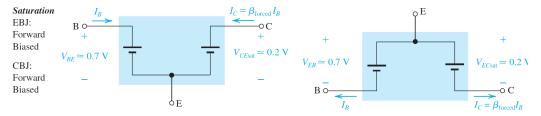


FIG 1. Simplified Models for the Operation of the BJT in DC Circuits

Use the following steps when analyzing BJT circuits with DC voltages:

Assume that the transistor is operating in active mode.

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- 4 If it is satisfied, the analysis is over.
- 5 If not, assume saturation mode and repeat the analysis like active mode.

In Fig. 2, if  $\beta = 100$  and  $V_{BE} = 0.7 V$ , which mode is the transistor operating in?

 Using Kirchhoff's Voltage Law (KVL) on the base-emitter loop (Equation (1))

$$4V = V_{BE} + 3.3 \,\mathrm{k}\Omega I_E \tag{1}$$

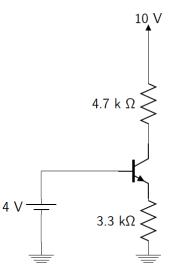


FIG 2. Example I

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Solving Equation (1) gives  $I_E = 1 mA$ 

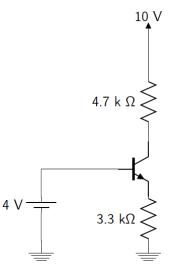


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- The base current  $I_B$  is calculated from its relationship to the emitter current

$$I_B = \frac{I_E}{\beta + 1} = 9.9\,\mu\text{A}$$

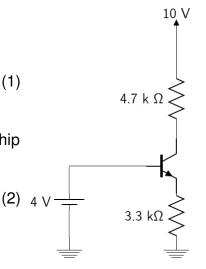


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• The collector current  $I_C$  is thus

$$I_C = \beta I_B = 0.99 mA$$

FIG 2. Example I

3.3 kΩ

 $(2)_{4}$ 

(3)

 $10 \$ 

■ To know the mode of operation of the transistors, we need to know *V*<sub>CE</sub>.

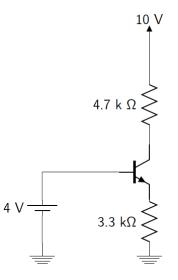


FIG 3. Example I

- To know the mode of operation of the transistors, we need to know  $V_{CE}$ .
- V<sub>CE</sub> is obtained by applying KVL on the CE loop as shown in Equation (4):

$$V_{CE} = 10V - 4.7 \,\mathrm{kV}I_C - 3.3 \,\mathrm{kV}I_E = 2.047V$$
 (4)

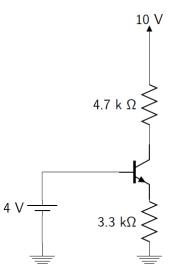


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• Since  $V_{CE} > V_{CEsat}$ , it is operating in active mode.

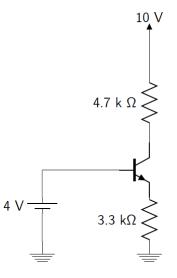
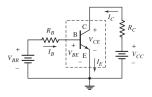
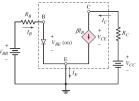


FIG 3. Example I

We will assume that the BEJ is forward biased, so the voltage drop across that junction is the cut-in or turn-on voltage V<sub>BE</sub>(on).



(a) npn transistor common-emitter

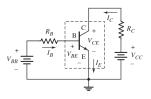


(b) dc equivalent circuit.

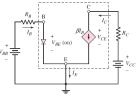
**FIG 4. Common emitter**—Transistor equivalent circuit is shown within the dotted lines with piecewise linear transistor parameters.

- We will assume that the BEJ is forward biased, so the voltage drop across that junction is the cut-in or turn-on voltage V<sub>BE</sub>(on).
- The base current is given in Equation (5)

$$I_B = \frac{V_{BB} - V_{BE}(on)}{R_B}$$
(5)



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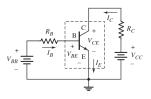
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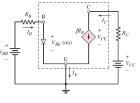
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(5)

• Equation (5) implies that  $V_{BB} > V_{BE}(on)$ —which means that  $I_B > 0$ . Otherwise,  $V_{BB} < V_{BE}(on)$ , the transistor is OFF and  $I_B = 0$ .



(a) npn transistor common-emitter

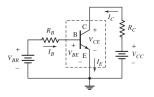


(b) dc equivalent circuit.

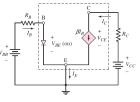
**FIG 4. Common emitter**—Transistor equivalent circuit is shown within the dotted lines with piecewise linear transistor parameters.

The collector current is given
Equation (6)

$$I_C = \beta I_B \tag{6}$$



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**FIG 5. Common emitter**—Transistor equivalent circuit is shown within the dotted lines with piecewise linear transistor parameters.

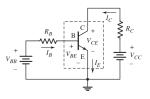
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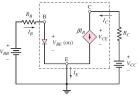
Kirchhoff's voltage law allows to compute V<sub>CC</sub> and V<sub>CE</sub>

$$V_{CC} = I_C R_C + V_{CE} \tag{7}$$

$$V_{CE} = V_{CC} - I_C R_C \tag{8}$$



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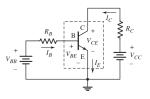
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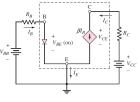
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• Equation (8) implicitly assumes that  $V_{CE} > V_{BE}(on)$ —which means that the BCJ is reverse biased and the transistor is the forward active mode



(a) npn transistor common-emitter

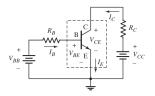


(b) dc equivalent circuit.

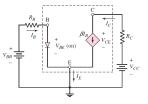
**FIG 5. Common emitter**—Transistor equivalent circuit is shown within the dotted lines with piecewise linear transistor parameters.

The power dissipated in the transistor is given by Equation (9)

$$P_T = I_B V_{BE}(on) + I_C V_{CE} \quad (9)$$



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(b) dc equivalent circuit.

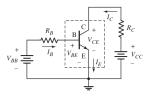
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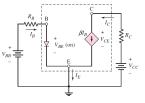
$$P_T = I_B V_{BE}(on) + I_C V_{CE} \quad (9)$$

■ However, in most cases I<sub>C</sub> ≫ I<sub>B</sub> and V<sub>CE</sub> > V<sub>BE</sub>(on). Thus, Equation (9) can be simplified as shown in Equation (10)

$$P_T \simeq I_C V_{CE} \tag{10}$$



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(b) dc equivalent circuit.

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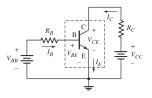
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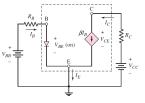
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The approximation in Equation (10), however, is not valid in the saturation mode.



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(b) dc equivalent circuit.

**FIG 6. Common emitter**—Transistor equivalent circuit is shown within the dotted lines with piecewise linear transistor parameters.

Calculate the base, collector, emitter currents, the  $V_{CF}$  voltage and the transistor power dissipation for the common-emitter circuit shown in Fig. 7. Assume  $\beta = 200$ and  $V_{BF}(on) = 0.7V$ 

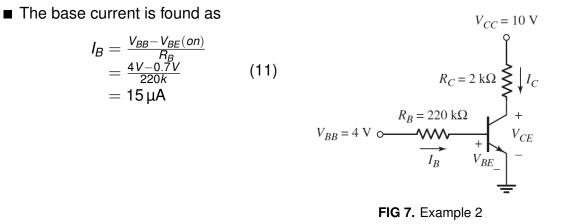


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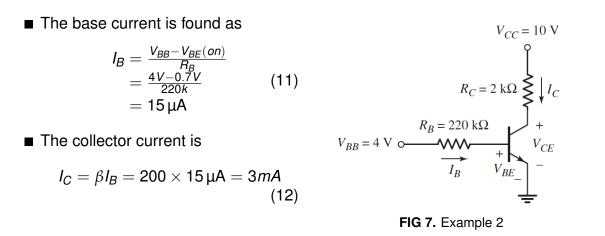
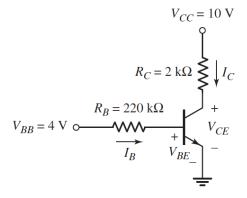


FIG 7. Example 2

#### ■ The emitter current is

$$I_E = (1 + \beta)I_B = 3.02mA$$
 (13)





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■ The collector-emitter voltage is

$$V_{CE} = V_{CC} - I_C R_C = 4V \quad (14)$$

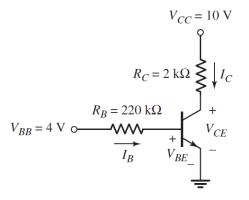


FIG 8. Example 2

The emitter current is

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■ The power dissipated is

$$P_T = I_B V_{BE}(on) + I_C V_{CE}$$
  
= 0.015 × 0.7 + 3 × 4 (15)  
= 12mW

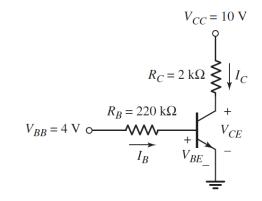


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= 0.015 × 0.7 + 3 × 4 (15)  
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■ Since *V*<sub>BB</sub> > *V*<sub>BE</sub>(*on*) and *V*<sub>CE</sub> > *V*<sub>BE</sub>(*on*), the transistor is biased in the forward-active mode.

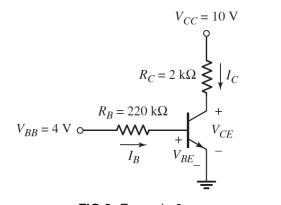
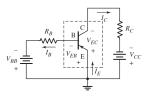
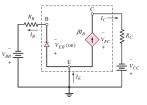


FIG 8. Example 2

In Fig. 9, the emitter is at ground potential, which means that the polarities of the V<sub>BB</sub> and V<sub>CC</sub> power supplies must be reversed compared to those in the npn circuit.



(a) pnp transistor common-emitter



(b) dc equivalent circuit.

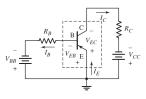
**FIG 9. Common emitter**—Transistor equivalent circuit is shown within the dotted lines with piecewise linear transistor parameters.

- In Fig. 9, the emitter is at ground potential, which means that the polarities of the V<sub>BB</sub> and V<sub>CC</sub> power supplies must be reversed compared to those in the npn circuit.
- The analysis proceeds exactly as before, and we can write:

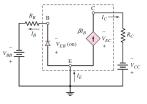
$$I_B = \frac{V_B B - V_{EB}(on)}{R_B} \qquad (16)$$

$$I_C = \beta I_B \tag{17}$$

$$V_{EC} = V_{CC} - I_C R_C$$



(a) pnp transistor common-emitter



(b) dc equivalent circuit.

(18) FIG 9. Common emitter—Transistor equivalent circuit is shown within the dotted lines with piecewise linear transistor parameters.

#### Example 3

Find  $I_B$ ,  $I_C$ ,  $I_E$  and  $R_C$  such that  $V_{EC} = \frac{1}{2}V^+$  for the circuit given in Fig. 10. Assume  $\beta = 100$  and  $V_{EB}(on) = 0.6V$ 

 $I_C = \beta I_B = (100)(5\mu A) \Rightarrow 0.5 \text{ mA}$ 

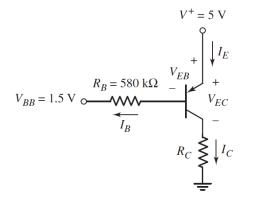
and the emitter current is

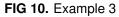
 $I_E = (1 + \beta)I_B = (101)(5\mu A) \Rightarrow 0.505 \text{ mA}$ 

For a C–E voltage of  $V_{EC} = \frac{1}{2} V^+ = 2.5 V$ ,  $R_C$  is

$$R_C = \frac{V^+ - V_{EC}}{I_C} = \frac{5 - 2.5}{0.5} = 5 \,\mathrm{k}\Omega$$

In this case,  $(V^+ - V_{BB}) > V_{EB}(on)$ . Also, because VEC > VEB(on), the pnp bipolar transistor is biased in the forward-active mode.





# The end